Velocity Motion Model (cont)

and of [xi] = [x]

center of circle

$$\left(\begin{array}{c} x^* \\ y^* \end{array} \right) \quad = \quad \left(\begin{array}{c} x \\ y \end{array} \right) + \left(\begin{array}{c} \lambda \sin \theta \\ \lambda \cos \theta \end{array} \right) \quad = \quad \left(\begin{array}{c} \frac{x+x'}{2} + \mu(y-y') \\ \frac{y+y'}{2} + \mu(x'-x) \end{array} \right)$$

where

$$\mu = \frac{1}{2} \frac{(x - x')\cos\theta + (y - y')\sin\theta}{(y - y')\cos\theta - (x - x')\sin\theta}$$

the ICC

vector

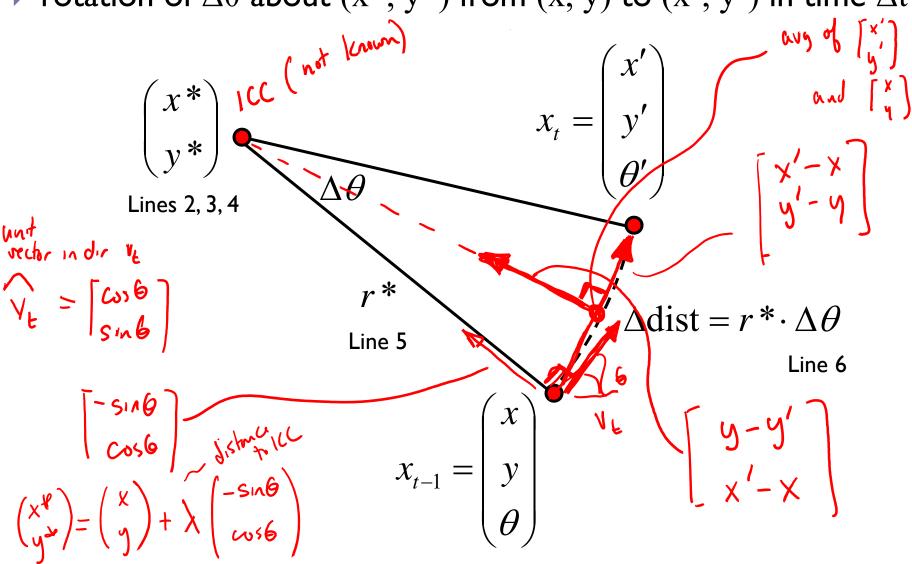
2 sets of equations

solve for M

r commanded velocités

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1:
             Algorithm motion_model_velocity(x_t,u_t):
                  \mu = \frac{1}{2} \frac{(x - x')\cos\theta + (y - y')\sin\theta}{(y - y')\cos\theta - (x - x')\sin\theta}
2:
                  3:
                  y^* = \frac{y + y'}{2} + \mu(x' - x)
4:
                  r^* = \sqrt{(x-x^*)^2 + (y-y^*)^2} distance to ICC
5:
                   \Delta \theta = \text{atan2}(y' - y^*, x' - x^*) - \text{atan2}(y - y^*, x - x^*) \ 
6:
                  \hat{v} = \frac{\Delta \theta}{\Delta t} r^*
7:
                  \hat{\omega} = \frac{\Delta \theta}{\Delta t}
8:
                   \hat{\gamma} = \frac{\theta' - \theta}{\Delta t} - \hat{\omega}
9:
                   return(prob)v - \hat{v}, \alpha_1 v^2 + \alpha_2 \omega^2) (prob(\hat{v} - \hat{\omega}, \alpha_3 v^2 + \alpha_4 \omega^2)
10:
                               (\mathbf{prob})(\hat{\gamma}, \alpha_5 \ v^2 + \alpha_6 \ \omega^2)
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rotation of $\Delta\theta$ about (x^*, y^*) from (x, y) to (x', y') in time Δt



• given $\Delta\theta$ and $\Delta dist$ we can compute the velocities needed to generate the motion

$$\hat{u_t} = \begin{pmatrix} \hat{v_t} \\ \hat{\omega}_t \end{pmatrix} = \begin{pmatrix} \Delta \text{dist }/\Delta t \\ \Delta \theta / \Delta t \end{pmatrix}$$
 Steps 7, 8 given the computed ICC

- notice what the algorithm has done
 - it has used an inverse motion model to compute the control vector that would be needed to produce the motion from x_{t-1} to x_t
 - in general, the computed control vector will be different from the actual control vector \boldsymbol{u}_t

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recall that we want the posterior conditional density

$$p(x_t \mid u_t, x_{t-1})$$

of the control action u_t carrying the robot from pose $x_{t\text{-}1}$ to x_t in time Δt

- > so far the algorithm has computed the required control action \hat{u}_t needed to carry the robot from position $(x \ y)$ to position $(x' \ y')$
 - the control action has been computed assuming the robot moves on a circular arc

- the difference is
- or expressed as an angular velocity

$$\gamma_{\text{err}} = \frac{\theta_{\text{err}}}{\Delta t}$$
$$= \frac{\theta' - \theta}{\Delta t} - \hat{\omega}$$

Velocity Motion Model

• the computed heading of the robot is assume what work with control vector
$$\hat{u} = \begin{bmatrix} \hat{v} \\ \hat{v} \end{bmatrix}$$
• the heading should be

$$\theta_{\text{err}} = \theta' - \hat{\theta}$$

$$= \theta' - \theta - \Delta \theta$$

Line 9. Eq 5.25, 5.28

> similarly, we can compute the errors of the computed linear

and rotational velocities

$$v_{\text{err}} = \hat{v} \cdot (\hat{v})$$

$$= v - \frac{\Delta \text{dist}}{\Delta t}$$

$$\omega_{\text{err}} = \hat{\omega} - \hat{\omega}$$

$$= \omega - \frac{\Delta \theta}{\Delta t}$$

if we assume that the robot has independent control over its controlled linear and angular velocities then the joint density of the errors is

$$p(v_{\text{err}}, \omega_{\text{err}}, \gamma_{\text{err}}) = p(v_{\text{err}}) \ p(\omega_{\text{err}}) \ p(\gamma_{\text{err}})$$
probability that we observe Ver 4 Werr 4 Yerr

what do the individual densities look like?

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the most common noise model is additive <u>zero-mean noise</u>, i.e.

- we need to decide on other characteristics of the noises
 - "spread" variance
 - "skew" skew
 - "peakedness" kurtosis
- typically, only the variance is specified
 - the true variance is typically unknown

the textbook assumes that the variances can be modeled as

$$var(v_{\text{noise}}) = \alpha_1 v^2 + \alpha_2 \omega^2$$

$$var(\omega_{\text{noise}}) = \alpha_3 v^2 + \alpha_4 \omega^2$$

$$var(\omega_{\text{noise}}) = \alpha_3 v^2 + \alpha_4 \omega^2$$

where the α_i are robot specific error parameters

lacktriangle the less accurate the robot the larger the $lpha_i$

- a robot travelling on a circular arc has no independent control over its heading

$$\theta' = \theta + \hat{\omega} \, \Delta t$$

- the heading must be tangent to the arc $\theta' = \theta + \hat{\omega} \, \Delta t$ because the heading must be tangent to the arc because the heading must be with the heading must be tangent to the arc heading must be tangent to the arc heading must be with the heading must be tangent to the arc heading must be with the heading must be with velocity ω
 - thus, we assume that the final heading is actually given by

$$\theta' = \theta + \hat{\omega} \, \Delta t + \hat{\gamma} \, \Delta t$$
 Eq 5.14 readon in place where $\hat{\gamma}$ is the angular velocity of the robot spinning in place

the book assumes that

It $\hat{\gamma} = 0 + \gamma_{\text{noise}}$ actual velocity noise

where

$$var(\gamma_{\text{noise}}) = \alpha_5 v^2 + \alpha_6 \omega^2 \qquad \text{Eq 5.15}$$

we now have assumed distribution of
$$\hat{v}$$
, $\hat{\omega}$, $\hat{\gamma}$